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Heat flux from magmatic hydrothermal systems related to availability of fluid recharge

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Magmatic hydrothermal systems are of increasing interest as a renewable energy source. Surface heat flux indicates system resource potential, and can be inferred from soil $CO₂$ flux measurements and fumarole gas chemistry. Here we compile and reanalyze results from previous $CO₂$ flux surveys worldwide to compare heat flux from a variety of magma-hydrothermal areas. We infer that availability of water to recharge magmatic hydrothermal systems is correlated with heat flux. Recharge availability is in turn governed by permeability, structure, lithology, rainfall, topography, and perhaps unsurprisingly, proximity to a large supply of water such as the ocean. The relationship between recharge and heat flux interpreted by this study is consistent with recent numerical modeling that relates hydrothermal system heat output to rainfall catchment area. This result highlights the importance of recharge as a consideration when evaluating hydrothermal systems for electricity generation, and the utility of $CO₂$ flux as a resource evaluation tool.

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1. Introduction

A common model of a magmatic hydrothermal system consists of a convecting cell of fluid. Meteoric water exchanges heat with a magmatic body at depth then rises toward the surface through permeable rock formations as a high-temperature plume of low density water, steam and gas (mostly $CO₂$). Most of the rising steam condenses in the shallow subsurface, and the resulting liquid condensate is discharged from the system either by lateral outflow ([Chiodini et al., 1996, 2005](#page-10-0)), or evaporation ([Chiodini et al., 2005; Hochstein and Bromley, 2005; Werner](#page-10-0) [et al., 2006](#page-10-0)). A proportion of the condensate may recycle back into the system through a "heat-pipe" mechanism ([Hochstein and Bromley,](#page-10-0) [2005](#page-10-0)). Water discharged from the system (according to the above processes) is typically recharged at the margins by meteoric water [\(Giggenbach, 1995; Dempsey et al., 2012\)](#page-10-0), or seawater in some coastal

Corresponding author. Tel.: $+64211045333$. E-mail address: mhar098@aucklanduni.ac.nz (M.C. Harvey). settings ([Sveinbjornsdottir et al., 1986; Parello et al., 2000; Dotsika](#page-10-0) [et al., 2009\)](#page-10-0). In many systems, magmatic water is a minor component of recharge ([Giggenbach, 1995](#page-10-0)). For most systems examined here, water is predominantly of meteoric origin. The quiescent-state heat flow from the system is useful for volcanic hazard monitoring, where a sudden increase in heat flow could precede a period of volcanic unrest. Heat flow evaluation is also useful for exploration of hydrothermal energy resources [\(Hochstein and Sudarman, 2008\)](#page-10-0); magmatic hydrothermal systems are of increasing interest as low carbon sources of base load electricity [\(Chamorro et al., 2012](#page-10-0)).

When the $CO₂/H₂O$ (unitless mass ratio) of the rising plume is known from fumarole gas analysis, and soil $CO₂$ flux can be quantified at the surface (using a portable $CO₂$ flux meter), the two can be combined to provide a proxy for heat flow, usually reported as megawatts (MW) ([Brombach et al., 2001; Chiodini et al., 2005; Fridriksson et al.,](#page-9-0) [2006; Hernández et al., 2012; Rissmann et al., 2012\)](#page-9-0). The geostatistical methods used to quantify soil $CO₂$ flux were previously explored and compared [\(Lewicki et al., 2005](#page-10-0)). Accordingly, fumarole chemistry provides complementary information to $CO₂$ flux measurements (i.e. by allowing $CO₂$ flux to be used as a proxy for heat flow). However, in

order to compare the intensity of heat flow from various volcanic and hydrothermal systems it is also useful to consider heat flux $(MW/km²)$, as distinct from heat flow (MW). Although the terms are often (erroneously) used interchangeably, heat flux is heat flow normalized to unit area ([Bird et al., 1960\)](#page-9-0).

Hydrothermal systems are generally characterized according to a number of factors including geochemistry [\(Giggenbach, 1996\)](#page-10-0), reservoir phase (liquid or vapor), temperature, lithology, and structural setting ([Henley and Ellis, 1983](#page-10-0)). Here we compile and reanalyze results from 22 hydrothermal areas representing a wide variety of settings. The objective is to determine how $CO₂$ flux, $CO₂/H₂O$ and the associated heat flux vary according to structural setting, reservoir phase, recharge source and recharge availability. Refer to Table 1 for a detailed summary of the physical and chemical characteristics of these systems. Hydrothermal studies were included on the basis that they provided both system $CO₂/H₂O$, and mapping of the hydrothermal $CO₂$ flux and a total $CO₂$ flow, allowing an estimate of heat flow.

Table 1

System setting.

2. Methods

The data provided in [Table 4](#page-8-0) is used to construct [Fig. 1.](#page-2-0) The data for 9 of the 22 systems in [Table 4](#page-8-0) comes from a previous study of $CO₂$ flux and fumarole analysis for a variety of hydrothermal systems ([Chiodini et al.,](#page-10-0) [2005\)](#page-10-0). Our study expands the previous study with the addition of new systems, and by considering the relationship between system heat flux and system setting.

Where possible, we have adopted the methodology of the earlier study so additional systems can be included and meaningfully compared (refer to Notes in [Tables 2 and 3](#page-3-0) for exceptions). This methodology provides the mean soil diffuse $CO₂$ flux of diffuse degassing structures (DDS) present within the various systems. DDS correspond to discrete areas of anomalous $CO₂$ flux, commonly associated with areas of high permeability (faults). The methodology delineates DDS areas using sequential Gaussian simulation; for most surveys, DDS are defined as areas of anomalous $CO₂$ flux where simulated flux values

^a Based on isotopic data from reservoir fluid.

b Dominant phase of the reservoir underlying survey area.

 ϵ Temperature of the reservoir underlying survey area.

^d Fumarole gas rich in acid magmatic gases (SO_{2,} HCl, HF) in survey area [\(Chiodini et al., 1995](#page-10-0)).

^e Fumarole chemistry arc/mantle type based on relative N₂, He, and Ar contents [\(Giggenbach, 1996](#page-10-0)).

^f Based on m

^g Based on chloride:boron ratio of thermal waters [\(Inguaggiato et al., 2000\)](#page-10-0).

Fig. 1. CO₂/H₂O versus log mean CO₂ flux for hydrothermal systems (data from [Table 4\)](#page-8-0). Solid purple line is line of best fit (excludes seawater recharged systems) ($R^2 = 0.91$). Error bars show the uncertainty resulting from fumarole measurements (vertical), or survey methodology (horizontal). (For interpretation of the references to color in this figure legend, the reader is referred to the web version of this article.)

have a >50% probability of exceeding twice the mean background (biogenic) flux ([Chiodini et al., 2005\)](#page-10-0). Some surveys were confined to thermal ground with little or no vegetation. In these cases the DDS area was assumed to be where $CO₂$ fluxes exceeded zero; the biogenic flux was assumed to be negligible (refer [Tables 2 and 3\)](#page-3-0). The uncertainty of the $CO₂$ flux estimate was computed from the simulation results, and found to be a function of $CO₂$ flux measurement density. The measurement density defined by number of measurements falling in the area contained by circle with radius equal to the range of the $CO₂$ flux variogram (circle range area (CRA)) ([Cardellini et al., 2003\)](#page-10-0). Raw data from recent $CO₂$ flux surveys at Ohaaki, Rotokawa, White Island (New Zealand) and San Jacinto (Nicaragua) were reprocessed using this approach (refer [Tables 2 and 3](#page-3-0)).

Summary data from a variety of surveyed hydrothermal areas are tabulated [\(Table 4](#page-8-0)). The calculated mean $CO₂$ flux for the various DDS areas is plotted against $CO₂/H₂O$ ratios (from fumarole or deep well gas analysis) for each area on a log–log plot (Fig. 1). For most DDS considered here, the contribution of focused venting from fumaroles inside the DDS has been previously reported or is assumed minor $\left($ < 10%). [Table 4](#page-8-0) and Fig. 1 include the contribution of focused venting. Mean $CO₂$ flux error bars are larger (\pm 50%) than previously used (\pm 30%) [\(Chiodini et al., 2005\)](#page-10-0), to allow for the added uncertainty in this contribution. There are no hot, neutral chloride springs within the studied DDS areas, so no contribution of deep reservoir liquid outflows to the surface heat flux.

Data points are color coded according to the hydrothermal reservoir type (liquid, vapor dominated, or vapor core: Section 3.1). Because heat flux is simply the product of $CO₂$ flux and fumarole $H₂O/CO₂$, straight lines of constant heat flux (50 and 500 MW $km⁻¹$, assumes steam condensation at 1 bar and 12 °C) can be conveniently represented in Fig. 1. These lines encompass most of the data points. Error bars show the inherent uncertainty in fumarole measurements due to condensation processes (negative vertical bars), and the determination of mean $CO₂$ flux (horizontal bars)([Chiodini et al., 2005](#page-10-0)). The rationale for assumptions, uncertainty, and other details of the method are provided in [Tables 2 and 3](#page-3-0).

3. Results and discussion

3.1. Variations in mean heat flux

The relatively narrow range of heat fluxes for most of the systems plotted here is consistent with previous observations that heat flow for a variety of high temperature, meteorically recharged systems of similar areal extent (i.e. approximate heat flux) fall within a single order of magnitude [\(Weir, 2009](#page-10-0)). The range is narrow relative to the range of permeabilities known to exist in hydrothermal reservoirs, which extend over several orders of magnitude [\(Weir, 2009\)](#page-10-0); if permeability were the primary constraint on system heat output, then we would also expect to observe a range of heat fluxes that span several orders of magnitude, but this is not the case.

The factors limiting heat flux from hydrothermal systems were investigated using a 1-D analytical model of heat and mass transfer for a hypothetical, meteorically recharged, convecting system ([Weir, 2009](#page-10-0)). Input parameters for the model included water infiltration rates, rainfall catchment area and enthalpy of the rising plume, giving system heat flow as output. The relationship between rainfall catchment and heat flow was explored further using 3-D numerical modeling of hydrothermal system up-flow and catchment areas for multiple systems [\(Dempsey et al., 2012](#page-10-0)). This study showed heat flows from individual systems are proportional to catchment area, in agreement with the 1- D analytical model [\(Weir, 2009\)](#page-10-0). The local meteoric recharge source

Table 2 Survey methods and geostatistics.

(see Fig. 3a, [Lowenstern et al. \(2012\)](#page-10-0)).

Table 2 (continued)

Location	# Meas.	Survey area ^a	DDS areab	Meas. density ^c	Meas. spacing ^d	CRA (km ²) ^e	\boldsymbol{n} $(CRA)^f$	Range $(m)^g$	ESD $(\pm \%)^h$	Notes
Krafla	3095	2.50	0.63	1238	grid $(25 \times 50 \text{ m})$				30	All $CO2$ flux survey data from Dereinda (2008). DDS area and associated mean $CO2$ flux was determined using the graphical statistical approach (GSA) (Chiodini et al., 1998; Dereinda, 2008).
Rotokawa	2545	1.40	0.75	1818	Irregular grid: 5-20 m spacing	0.091	165	170	7	DDS area is the sum of 5 DDS sub-areas at Rotokawa (Bloomberg et al., 2012). DDS sub-areas were determined from SGS probability maps (probability \geq 0.5), where flux exceeded twice the mean biogenic flux (10 g m ⁻² d ⁻¹). Range is the average of variogram ranges for the 5 sub-areas.
Karapiti	105	0.35	0.35	300	Approx. regular grid $(25-50 \text{ m})$				30	Survey results from Werner et al. (2004). DDS area was assumed to be the entire survey area. $CO2$ flux was determined from total $CO2$ flow (Grid Volume tool in Surfer®) and the DDS area $(CO2 flux = CO2 flow • survey area-1).$
Ischia, Donna Rachele	336	0.86	0.06	390	Random	0.080	31	160	18	Survey results from Chiodini et al. (2005).
Reykjanes	352	0.23	0.11	1564	Regular Grid $(25 \times 25 \,\mathrm{m})$	0.053	83	130	11	All data from Fridriksson et al. (2006). ESD $(\pm 11\%)$ calculated based on sample density and Variogram Range.

^a Survey area (km^2) : total CO₂ flux survey area
^b DDS area (km^2) : upless stated otherwise (see

ª Survey area (km²): total CO₂ flux survey area.
^b DDS area (km²): unless stated otherwise (see Notes column) the diffuse degasing structure area is determined from SGS probability maps (prob. ≥ 0.5) where flux ex mean biogenic flux [\(Chiodini et al., 2005](#page-10-0)).

^c Meas. density: CO₂ flux measurements per square km.
^d Meas. spacing: pattern of measurements.

^e CRA (km²): circle range area – circle with radius equal to the range of the CO₂ flux variogram (Cardellini et al., 2003).
^f *n* (CRA): number of CO₂ flux measurements inside the CRA (Cardellini et al., 2003).

^g Range (m): range of the CO₂ flux variogram [\(Cardellini et al., 2003\)](#page-10-0).
^h ESD (\pm %): estimated standard deviation. Assumed to be \pm 30% [\(Chiodini et al., 2005\)](#page-10-0) unless derived from sample density and variogram r

for these systems was determined by isotope analysis (see collation of isotope studies: [Dempsey et al., 2012](#page-10-0)).

Both studies acknowledge that the models do not consider the effect of surface topography, but will be strongly affected by this factor [\(Weir,](#page-10-0) [2009; Dempsey et al., 2012\)](#page-10-0). For example, surface topography will affect the direction and magnitude of groundwater flows; all else being equal, hydrothermal systems located in a basin, and coastal systems, would receive higher lateral recharge than equivalent systems located beneath a cone. Accordingly, basinal systems should in general have a greater supply of water to serve as the medium for convective heat flow.

Indeed, the geographic distribution of many of the hydrothermal systems in the Taupo Volcanic Zone (New Zealand) would appear to be constrained by recharge availability, including Karapiti (Wairakei), Rotokawa and Ohaaki from this study. [Fig. 2](#page-9-0) shows the distribution of these systems overlaid on an elevation model of the area; it is striking that most of the systems fall along the Waikato River (9 out of 13), which is the primary hydrological drainage channel and topographic low for the Taupo graben.

The systems with the two highest heat fluxes are Reykjanes (1048 MW km⁻²) and Ischia (766 MW km⁻²). According to the above discussion, a simple explanation is that both systems receive relatively high recharge. Indeed, both systems are predominantly seawater charged ([Sveinbjornsdottir et al., 1986; Inguaggiato et al., 2000\)](#page-10-0), so have a potentially unlimited water supply.

At the other extreme, Vesuvio, Italy (55 MW $\rm km^{-2}$) has one of the lowest heat fluxes. At Vesuvio, heat flux is not limited by reservoir temperature (360 °C, see [Table 1\)](#page-1-0), but by topography. The large Vesuvio cone deflects meteoric recharge away from the system in all directions over a wide $(>100 \text{ km}^2)$ area [\(Federico et al., 2002](#page-10-0)). Accordingly, there is probably little meteoric water available to recharge the system and facilitate convective heat flow.

Heat fluxes for DDS at Pantelleria, Italy, and Nisyros, Greece, are very low (<70 MW km $^{-2}$). Stefanos DDS at Nisyros (166 MW km $^{-2}$) comprises only a minor proportion of the total DDS area (12%), so is not representative of the heat flux at Nisyros, and the overall heat flux there is very low ([Caliro et al., 2005](#page-10-0)). Pantelleria and Nisyros both have very low rainfall (≤500 mm yr−¹ precipitation) [\(Grassi et al.,](#page-10-0) [1995; Drouza et al., 2007\)](#page-10-0), and isotope geochemistry indicates a proportion of seawater in both reservoirs [\(Parello et al., 2000; Dotsika et al.,](#page-10-0) [2009\)](#page-10-0). The low heat flux observed at Nisyros and Pantelleria demonstrates that seawater recharge does not always equate to high heat flux (cf. Reykjanes). Instead, seawater recharge only provides the potential for high heat flux where other factors are not limiting (i.e. permeability and/or heat source).

The line of best fit [\(Fig. 1\)](#page-2-0) indicates a general trend toward lower heat flux for vapor core systems and possibly vapor dominated systems. Mud Volcano and Hot Spring Basin (HSB), Yellowstone, plot among the vapor core systems with moderate heat fluxes. However both systems are vapor dominated, rather than vapor core ([Werner et al., 2008b](#page-11-0)). Vapor dominated systems can develop in locations where recharge is limited by low permeability or other factors [\(White et al., 1971; Allis,](#page-11-0) [2000\)](#page-11-0). They differ from vapor core systems because they may have a neutral liquid reservoir at depth (beneath the vapor zone) ([White](#page-11-0) [et al., 1971](#page-11-0)).

Vapor core and vapor dominated systems are often associated with high relief terrain (Fournier, [1989; Allis, 2000\)](#page-10-0). For example, Vesuvio and Vulcano are stratovolcanoes. Mud Volcano and Hot Spring Basin (HSB) are located within the relatively high elevation east-central plateau of Yellowstone Park; the vapor dominated nature of these systems was previously attributed to their high elevation ([Fournier, 1989\)](#page-10-0). High relief terrain tends to drain liquid water laterally away to lower elevation catchments; higher elevation geothermal areas often exhibit deep water tables and vapor zones. Accordingly, the trend towards lower heat flux for some vapor core and vapor dominated systems may be explained in terms of recharge.

Alternatively, the moderate heat fluxes at White Island and Masaya may be partly an artifact of sampling bias that results in less measurement in the least accessible areas of vapor core systems, where the most focused emissions are expected; both systems have focused

Table 3 (continued)

 $^{\text{a}}$ DDS area (km²); unless stated otherwise (see Notes column) the diffuse degasing structure (DDS) area is determined from SGS probability maps (prob, ≥ 0.5) where flux exceeds twice the mean biogenic flux (Ch

^b CO₂ flow (diff.): geothermal CO₂ flow (tons d⁻¹) for the anom. area from soil diffuse flux survey.

 ϵ CO₂ flow (focus): estimated geothermal CO₂ flow (tons d⁻¹) from fumaroles within the DDS (s).

^d Total CO₂ flow (ton d⁻¹): CO₂ flow (diff.) + CO₂ flow (focus).

^e Backgr. stat. (g m⁻² d⁻¹): biogenic CO₂ flux estimated using statistical method ([Chiodini](#page-10-0) et al., 1998).

f Backgr. contr. area (g m⁻² d⁻¹): biogenic CO₂ flux estimated from a set of measurements in a non-geothermal area ([Chiodini](#page-10-0) et al., 2007).

^g Backgr ¹³C (g m^{−2} d^{−1}): biogenic CO₂ flux estimated on the basis of the carbon (¹³C) isotopic signature ([Chiodini](#page-10-0) et al., 2008).

^h CO₂ flux (tons km⁻² d⁻¹): total CO₂ flow/DDS area.

 $\frac{1}{1}$ CO₂ flux error ($\pm \frac{1}{2}$): est. error for CO₂ flux. Assumed to be 30% ([Chiodini](#page-10-0) et al., 2005), unless large CO₂ flow (focus) is probable.

^j CO2/H2O:CO2/H2O mass ratio of the rising vapor plume. Determined from fumarole or deep well gas measurements.

k CO₂/H₂O error (%); est. error for CO₂/H₂O. Assumed to be −50% ([Chiodini](#page-10-0) et al., 2005) unless based on deep well gas analysis.

Compilation of soil diffuse $CO₂$ flux survey results.

a Area - DDS area where CO₂ flux has ≥50% probability of exceeding twice the mean background (biogenic) flux, except where stated otherwise (refer to Notes in [Tables 2 and 3](#page-3-0) for details).

^b FCO₂ – flow of hydrothermal CO₂ within DDS (diffuse + focused venting).

 $\frac{1}{10}$ CO₂/H₂O – mass ratio of the rising vapor plume, determined from fumarole or deep well measurements.
 $\frac{1}{10}$ CO₂/H₂O – mass ratio of the rising vapor plume, determined from fumarole or deep well meas was derived from the enthalpy of liquid water at reservoir temperature (212 °C).

central plumes that were not included in the survey because the areas are inaccessible. At White Island the central plume underlies an acidic crater lake [\(Werner et al., 2008a](#page-10-0)). At Masaya, survey measurements were conducted on the flanks of the volcano ([Lewicki et al., 2003](#page-10-0)).

3.2. Geothermal electric power plants and heat flux

The low power density (electrical capacity per unit area of reservoir) of geothermal power plants supplied by vapor dominated reservoirs at the Geysers (USA) and Lardarello (Italy) was noted previously, and attributed to lower recharge relative to other systems where power plants exist ([Allis, 2000\)](#page-9-0). Electrical output at these and most other geothermal power plants (both vapor and liquid dominated) is now routinely supported by artificial recharge (injection) of fluids into the productive reservoir ([Stefansson, 1997;](#page-10-0) [Kaya et al., 2011](#page-10-0)).

It is interesting to note the mean electrical capacity of 53 hightemperature geothermal fields (16.2 MW electric km−²) ([Wilmarth](#page-11-0) [and Stimac, 2014](#page-11-0)). Assuming a typical energy conversion efficiency of 0.1 from thermal energy to electric, 16.2 MW electric km^{-2} equates to 162 MW km−² [\(Ghoniem, 2011; Zarrouk and Moon, 2014](#page-10-0)). This value is comparable to the mean heat flux for hydrothermal systems determined in this study (198 MW km⁻², excluding seawater systems Reykjanes and Ischia). These values are of the same order of magnitude as the global average solar heat flux captured by the Earth's surface water during evaporation (80 MW km^{-2}), then released during condensation (rain) ([Trenberth et al., 2009\)](#page-10-0).

Energy fluxes associated with phase changes in water (i.e. liquid to vapor or vice versa) are related to changes in specific enthalpy of the fluid, which allows heat flux (e.g. MW km $^{-2}$) and water flux (e.g. tons $\rm km^{-2}$ day $^{-1}$) to be used interchangeably. Further, such changes are relatively insensitive to temperature; the enthalpy change associated with the condensation of steam (100 °C) to ambient liquid water (12 °C) in

hydrothermal areas (2624 kJ kg⁻¹), is similar to that associated with the evaporation of Earth's surface waters (~2260 kJ kg⁻¹). Accordingly, the mean heat flux for meteorically recharged hydrothermal systems determined in this study (198 MW km⁻²) may be a manifestation of the available incoming solar energy flux, the ultimate driver of the hydrological cycle.

3.3. Variations in CO₂ flux and CO₂/H₂O

In order to determine the cause of variations in $CO₂$ flux and $CO₂$ / H₂O, we have considered the distribution of flux measurements [\(Fig. 1\)](#page-2-0) in terms of the reservoir dominant phase and geological setting of the individual systems ([Table 1\)](#page-1-0). With the notable exception of Krafla, vapor core systems (red markers in [Fig. 1](#page-2-0)) all plot with high $CO₂$ fluxes and $CO₂/H₂O$ ratios. The high $CO₂$ flux results from a degassing magma at depth, where no deep liquid reservoir is present to remove $CO₂$ during ascent. This contrasts with liquid dominated systems, where a greater proportion of the ascending $CO₂$ is dissolved in the liquid as HCO_3^- . The HCO_3^- may subsequently exit the system via lateral outflow, or be precipitated in the reservoir as calcite [\(Giggenbach, 1981](#page-10-0)). Vapor dominated systems at Yellowstone (Mud Volcano and Hot Spring Basin) also have high $CO₂$ flux, consistent with a deep, small liquid reservoir that has limited capacity to remove CO₂.

Krafla, despite being a vapor core system, has low $CO₂$ fluxes and $CO₂/H₂O$ because of its position in newly formed basalt crust; Icelandic magmas are deeply sourced and depleted in volatiles, including CO₂. Similarly, the low CO₂/H₂O of Karapiti (Wairakei) relative to Ohaaki and Rotokawa was previously attributed to the depth of the degassing magma, and the associated depletion of magmatic volatiles [\(Giggenbach, 1995\)](#page-10-0). This would also explain the low $CO₂$ flux of Karapiti relative to Ohaaki and Rotokawa.

Fig. 2. Location of hydrothermal fields (red areas) in the Taupo Volcanic Zone overlaid on a satellite digital terrain model (WGS84). Darker shading indicates lower elevation. Field boundaries are based on shallow electrical resistivity data (Bibby et al., 1995). (For interpretation of the references to color in this figure legend, the reader is referred to the web version of this article.)

4. Conclusions

Our results show that variations in the $CO₂$ flux, $CO₂/H₂O$, and associated heat flux seen in the systems examined here may be explained in terms of the specific geological and hydrological setting of the systems. Our results indicate that recharge availability exerts a strong control over the location of hydrothermal systems, and in some cases may constrain the heat flux from hydrothermal systems (i.e. vapor systems). Recharge is in turn governed by permeability, structure, rainfall, topography, and possibly proximity to an unlimited supply of water such as the ocean. The relationship between recharge and convective heat flux interpreted by this study is consistent with recent numerical modeling that relates system heat output to rainfall catchment area.

This finding has implications for the development of hydrothermal electricity, currently slowed by the economic risks of exploration. We identify recharge availability as an important factor in resource prospectively, and the utility of the $CO₂$ flux survey technique for geothermal resource evaluation.

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